

Hydrogeological modelling for the watershed management of the Mar Menor coastal lagoon (Spain)

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ABSTRACT

The Mar Menor is the largest lagoon along the Spanish Mediterranean coast. It suffers from eutrophication and algal blooms associated with intensive agricultural activities and urban pressure in the surrounding Campo de Cartagena plain. A balanced discharge of groundwater, carrier of algal nutrients such as nitrate, is essential to ensure the integrity of the coastal lagoon and the availability of groundwater resources inland. We here present a 3D hydrogeological model of the unconfined Quaternary aquifer that discharges into the lagoon. The model couples both surface water balance and groundwater dynamics and has been calibrated

25 to available data in the period 2000–2016. The calibrated model allows understanding of the current state
26 of the aquifer and its link to the lagoon. The potential discharge has been quantified in both space and time
27 and falls between 69.5 and 84.9 hm³/yr during dry and wet periods, respectively (with values of nitrate
28 discharge of 11.4–11.8 Mkg/yr in the absence of aquifer sink terms, e.g., leakage to deeper aquifers and
29 pumping from groundwater wells). The predictive capabilities of the calibrated model can be used to test
30 the impact of different integrated management scenarios on the surface-groundwater dynamics of the
31 catchment. Three plausible management scenarios are proposed that include localized and distributed
32 groundwater pumping (drains and groundwater wells, respectively). Results show the effectiveness of the
33 scenarios in reducing the groundwater and nitrate discharge into the lagoon. The disadvantages of the
34 proposed scenarios, including potential seawater intrusion, need to be balanced with their relative merits
35 for the sustainable development of the region and the survival of the Mar Menor ecosystem. The modelling
36 approach proposed provides a valuable tool for the integrated and holistic management of the Campo de
37 Cartagena-Mar Menor catchment and should be of great interest to similar hydrological systems with high
38 ecological value.

39

40 **Keywords:** 3D hydrogeological modelling, integrated watershed management, eutrophication, Campo de
41 Cartagena, Mar Menor coastal lagoon.

42

43

44 **1. Introduction**

45 Coastal lagoons are shallow coastal water bodies, separated from the ocean by sedimentary or anthropic
46 barriers, but connected to it (at least temporarily) by one or several inlets (Kjerfve, 1994, Duck and da Silva,
47 2012). They are important ecosystems (see e.g., Isla, 1995) and sustain numerous economic activities like
48 fishery and tourism. However, their location, generally near densely populated areas, and the often poor
49 water renewal make coastal lagoons highly vulnerable. Amongst other threats, eutrophication has been
50 identified as a major concern over the last decades (Le Moal et al., 2019). Eutrophication of coastal lagoons

51 is a serious problem worldwide (see e.g., the cases of Ria Formosa, Portugal, Newton et al., 2003; Maryland,
52 US, Boynton et al., 1996; Sacca de Goro, Italy, Naidi and Viaroli, 2002; Lake Shinji, Japan, Nakamura and
53 Kerciku, 2000; Lagune de Thau, France, Mesnage and Picot, 1995; Rhode Island, US, Lee and Olsen,
54 1985). The input of nutrients to coastal lagoons contributes dramatically to algal blooms (Breininger et al.,
55 2017) that can reach levels of toxicity to wildlife and humans. Thus, eutrophication also causes negative
56 impacts on tourism and, correspondingly, on the economy (McCrakin et al., 2017). Anthropogenic activities
57 are the main sources of nutrients and are of two kinds, point source and diffuse. The point source
58 contribution of the surrounding hydrological surface network to eutrophication (e.g., after spills) has
59 received attention by the authorities and in the literature (e.g., Arellano-Aguilar et al., 2017; Velasco et al.,
60 2005). However, the diffuse contribution of submarine discharge of groundwater is usually ignored due to
61 the opacity of this process (Robinson et al., 2017).

62
63 Unconfined coastal aquifers play a key role in the eutrophication of coastal lagoons because they usually
64 control the submarine discharge of groundwater with transported chemicals (Dimova et al., 2017; Menció
65 et al., 2017). Thus, understanding the interactions between aquifer and lagoon in both seaward and landward
66 directions is critical for the sustainable management of water resources in coastal areas. For example, the
67 intensive pumping of groundwater may result in seawater intrusion, whereas the practice of intensive
68 agriculture may lead to the discharge of groundwater with a high chemical load (see e.g., Rodellas et al.,
69 2015). In regions where agriculture involves nitrogen (and to a lesser extent) phosphorous-based fertilizers,
70 unconfined coastal aquifers behave as buffers that introduce a time lag between the leaching of fertilizers
71 (Ascott et al., 2017) and their potential discharge into the lagoon (Gilmore et al., 2016; Vero et al., 2018).
72 Therefore, an accurate evaluation of the budget of fertilizers in groundwater is essential to forecast the
73 discharge of nutrients into the lagoon (and in general into other water bodies). Integrated numerical models
74 of surface/groundwater flow and contaminant transport are useful to that end. Unfortunately, the main
75 inputs to such models (e.g., the geometry of the system and its physical properties, forcing terms like
76 pumping rates) are highly uncertain and long-term monitoring of the aquifer (which is rarely available) is

77 required to build representative (in the sense of calibrated) models with predictive capabilities for the
78 integrated and sustainable management of surface water and groundwater resources.

79

80 The modelling of unconfined aquifers connected to coastal lagoons with poor water renewal (e.g., not
81 affected by tides) is a difficult task. At the watershed scale, the main forcing term inland, i.e., aquifer
82 recharge, usually exhibits wide spatio-temporal variability (Santos et al., 2012; Han et al., 2017; Rodríguez-
83 Gallego et al., 2017). At a smaller scale, the modelling of groundwater dynamics near to the coast is further
84 complicated by (1) aquifer heterogeneity, (2) evaporation of groundwater at shallow depths and of surface
85 water in wetlands, e.g., saltmarshes, and (3) variable-density effects (Werner et al., 2013). The interplay
86 between these factors is highly non-linear. For example, evaporation increases groundwater salinity, that
87 leads to salt accumulation (Shokri and Or, 2011) and to local density-driven effects, also aggravated by
88 aquifer heterogeneity, which controls the spatial distribution of submarine discharge. The experimental
89 evaluation of the separate contribution of these effects is difficult, even hardly possible. Numerical
90 modelling is often used to characterize the behaviour of such complex hydrological systems, regardless of
91 their scale. In addition, numerical models are useful to integrate all available information, and are therefore
92 well-suited and objective tools for decision-making, management of water resources and the planning of
93 future monitoring surveys (Candela et al., 2013).

94

95 Here, we present a numerical model to quantify the discharge of groundwater and nitrogen-based fertilizers
96 from an unconfined Quaternary aquifer into the Mar Menor coastal lagoon (SE Spain). The Mar Menor
97 lagoon and its watershed, the Campo de Cartagena plain, are one of the most representative examples of
98 highly anthropized area in the Mediterranean coast. The Mar Menor (literally translated as “The Small
99 Sea”), is actually the largest lagoon along the Spanish Mediterranean coastline and has been catalogued as
100 a protected area under several lists: (1) the Ramsar Convention of Wetlands (<https://rsis.ramsar.org/ris/706>),
101 (2) Special Protected Areas of Mediterranean Interest (<http://www.rac-spa.org/spami>), (3) the EU 79/409
102 Birds Directive, and (4) the Nature 2000 Network as a Site of Community Importance

103 (<http://www.mpatlas.org/mpa/sites/12699/>). The main land use in the surrounding area includes rainfed and
104 irrigated intensive agriculture that, along with high urban pressure, are the main contributors to the
105 eutrophication of the Mar Menor lagoon, which has already suffered recent episodes of algal bloom.
106 Groundwater discharge has recently been demonstrated to be the main source of nutrient-enriched water
107 (Jiménez-Martínez et al., 2016). Groundwater discharge is heterogeneous both in space and time, and in
108 quality and quantity due to the seasonality of crops and the unevenly distributed rainfall events (i.e., mainly
109 short rainstorms). Therefore, to better understand the link between discharge and eutrophication, it is
110 necessary to use a dynamic process-based numerical model that integrates both surface water and
111 groundwater dynamics. We have developed a novel 3D variable-density hydrogeological model to improve
112 the current understanding of the impact of (1) the chronic environmental stressors (i.e., increase in aquifer
113 recharge and the load of agrochemicals resulting from an increase in intensive agriculture in the area) and
114 (2) the anthropogenic perturbations (e.g., shallow drains parallel to the coastline) on discharge into the
115 coastal lagoon. The model is capable of reconstructing the discharge of groundwater over the last two
116 decades (October 2000–December 2016) and provides a reliable characterization of the current state of the
117 aquifer–lagoon system. We also use the model as a predictive tool to analyse the relative merits and
118 drawbacks of so-called mitigation measures, aimed at reducing the discharge of nutrients into the lagoon to
119 prevent a progressive decline and eventual collapse of the ecosystem. In particular, two so-called localized
120 scenarios involving current and newly designed drains to intercept more discharge, and a distributed
121 groundwater-pumping scenario were devised in close consultation with local authorities and stakeholders.

122
123 This paper is organized as follows. First, the study area, the model and the suggested scenarios are described
124 in detail. Second, results are presented and discussed. Finally, the paper ends with some conclusions about
125 the use of modelling techniques for the integrated management of surface water and groundwater resources
126 in coastal areas, and for designing mitigation measures to protect endangered ecosystems in coastal lagoons
127 under high anthropic pressure.

128

129 **2. Methodology**

130 **2.1. Study area**

131 The catchment of the Mar Menor coastal lagoon is the Campo de Cartagena plain (SE Spain), with a surface
132 area of 1316 km² (Figure 1a). The plain has a gentle slope towards the east (1%) and is surrounded by low
133 mountain ranges except in the east, where the lagoon is located. This region has a semi-arid climate with a
134 mean annual temperature of 18 °C, an average annual precipitation of 300 mm, and a potential
135 evapotranspiration of 1275 mm/yr (Sanchez et al., 1989). Rainfall is highly variable both in space and time,
136 and is unevenly distributed into a few intensive events, mainly during spring and autumn. Agriculture is the
137 main land use, both rainfed (including almond, winter cereals and olive, covering 6% of the area) and
138 intensively irrigated (including horticultural crops and citrus trees, 31% of the area). Drip irrigation is the
139 most extended practice (90%) due to water scarcity (Alcon et al., 2011). Historically, the water demand for
140 irrigation has been covered by the Tajo-Segura Water Transfer (T-S WT, established in 1979, <1/3 of the
141 demand) and groundwater pumping (<2/3). However, the unmet water demand for irrigation and the recent
142 development of tourism in the area has led to the construction of seawater desalinization plants. The high
143 operational costs of such plants has limited their use for irrigation (Lapuente, 2012; Martin-Gorriz et al.,
144 2014), forcing farmers to install small, privately owned, desalinization equipment to reduce the salinity of
145 the low quality pumped groundwater (Aparicio et al., 2017).

146
147 The surface hydrology network draining into the Mar Menor coastal lagoon consists of non-permanent
148 watercourses flowing only during (and shortly after) episodes of intense rain. Since the implementation of
149 T-S WT, groundwater levels have risen as a consequence of the irrigation return flows. This has made some
150 watercourses behave partially (close to the mouth) and temporally like small rivers (García-Pintado et al.,
151 2007) since the 1920s. The groundwater resource is provided by a sedimentary multi-layered system with
152 geological ages ranging from Neogene (Tortonian) to Quaternary. Overall, the hydrogeological system is
153 constituted by three deep confined aquifers of Tortonian, Messinian and Pliocene ages (from bottom to

154 top), and a Quaternary unconfined shallow aquifer (Jiménez-Martínez et al., 2012). The latter discharges
155 into the Mar Menor lagoon and is the object of this study. The Quaternary aquifer, highly polluted by
156 agrochemicals due to irrigation return flows, covers almost the entire Campo de Cartagena plain (Figure
157 1a). The high density of abandoned, poorly constructed (in the sense of leaky) deep wells induces cross-
158 formational groundwater flows and contamination of the confined deeper aquifers at the local scale
159 (Jiménez-Martínez et al., 2011; Baudron et al., 2013). At the regional scale, the spatio-temporal
160 distributions of groundwater levels in the shallow unconfined and in the deeper confined aquifers are
161 independent (García-Aróstegui et al., 2017).

162
163 The Mar Menor lagoon (Figure 1b) has a surface of 135 km² and a volume of 593 hm³, with mean depth
164 4.5 m and maximum depth <6.5 m. The lagoon is one of the largest in the Mediterranean basin (Perez-
165 Ruzafa et al., 2011, 2013) and the largest along the Spanish Mediterranean coast. It is separated from the
166 open sea by a 22-km-long sand bar (La Manga), although one natural inlet and two artificial channels allow
167 some water renewal (water velocity in the lagoon is lower than 0.03 m/s; García-Oliva et al., 2018). This
168 valuable ecosystem has been degraded over the last decades, with flora and fauna as bio-indicators of the
169 trophic changes (Perez-Ruzafa et al., 2007). Anthropogenic pressure on the lagoon is related to: (1) the
170 opening and dredging of artificial inlets in the sandbar, which have induced changes in the hydrodynamics
171 and water balance of the lagoon (so-called “Mediterraneanisation”, Perez-Ruzafa et al., 2009); (2) the acid
172 drainage of heavy metals from an abandoned mining area (Cartagena-La Unión mining district in Figure
173 1a; Jimenez-Carceles and Alvarez-Rogel, 2008); (3) the discharge of nutrients from both the surface water
174 network and groundwater (average nitrate concentration in the lagoon <1 mg/L, but with peaks up to 3.5
175 mg/L, Baudron et al., 2015; Velasco et al., 2005), a by-product of the intensive agricultural activity in spite
176 of the retention and degradation taking place in the saltmarshes surrounding the lagoon (Tercero et al.,
177 2017); and (4) the emerging input of organic contaminants of concern from agricultural activities and urban
178 water spills (Moreno-Gonzalez et al., 2015; Traverso-Soto et al., 2015). Past and current economic activities

179 have converted the Mar Menor lagoon, markedly oligotrophic in its natural regime, into a highly
180 eutrophicated ecosystem (Perez-Ruzafa et al., 2009), collaterally damaging other activities such as fishery
181 and tourism (Marcos et al., 2015). For a detailed review of the environmental stressors and impacts on the
182 Mar Menor lagoon, the reader is referred to Jiménez-Martínez et al. (2016).

183

184 **2.2. Model description**

185 A three-dimensional (3D) hydrogeological model was built that couples a surface water balance model with
186 a groundwater model. Compared to 2D models, 3D models require significantly more resources in terms of
187 CPU and data for their parameterization, calibration and validation. In exchange, 3D models allow density-
188 driven effects to be addressed, in this case at the interface between the unconfined aquifer and the lagoon.
189 The surface water balance and its main components were quantified with the open-source SPHY (Spatial
190 Processes in Hydrology) bucket-type modelling code (Terink et al., 2015), previously adapted for the study
191 region by Contreras et al. (2014, 2017). In this study, SPHY computes the main water balance components
192 and soil moisture dynamics at discrete soil layers and on a daily basis. The water balance at the root zone
193 is primarily controlled by soil moisture (i.e., the state variable), the inflows from precipitation and the main
194 water losses due to interception and actual evapotranspiration. The latter are driven by vegetation (satellite-
195 based vegetation greenness and fractional vegetation cover), root depth, water storage and soil texture.
196 Lateral fluxes in the vadose zone are neglected. This assumption is acceptable due to the smooth topography
197 in the studied area (i.e., about 90% with slopes <1%). As such, vadose flows are mainly attributed to capillary
198 forces, whose effect is minor and local. Therefore, the non-evapotranspired fraction of precipitation that
199 exceeds the storage capacity of the soil is computed as potential recharge to the shallow aquifer.

200

201 The main inputs to the SPHY model are both static and dynamic. The static inputs are terrain slope (derived
202 from a Digital Elevation Model) and the main hydraulic properties of the soil, which can be derived from
203 soil textural maps and pedotransfer functions (Wösten et al., 2001). The main dynamic inputs are derived

204 from climate data (precipitation and Penman-Monteith reference evapotranspiration) and satellite-based
205 vegetation data (Normalized Difference Vegetation Index -NDVI-, used as a surrogate of the vegetation
206 growth phenology and productivity). The main outputs of SPHY are evapotranspiration losses and aquifer
207 recharge, which is used as input to the 3D variable-density groundwater model. Groundwater flow is solved
208 with the open-source finite elements code SUTRA (Saturated-Unsaturated TRANsport, Voss and Provost,
209 2010). Aquifer properties (hydraulic conductivity and storativity) are heterogeneous and calibrated using
210 the Regularized Pilot Points Method (Alcolea et al., 2006), as implemented in the generic calibration
211 software PEST (Doherty, 2016).

212

213 **2.3. Model setup**

214 The surface water model encompasses a surface area of 2235 km² divided into 35,760 cells of 250 x 250 m
215 (a control volume of 62,500 m², the third dimension being the root depth). It is larger than the groundwater
216 model, which spans the Quaternary aquifer only, to account for surface runoff to other surrounding
217 watersheds. The meteorological data sets (precipitation and reference evapotranspiration) required to
218 simulate the period October 2000–December 2016 were obtained from the SIAM network
219 (<http://siam.imida.es/>), which includes 12 stations for the modelled area and 4 out of it (also used for the
220 calculation of isohyets; Figure 2a). Station-based measurements were spatially interpolated using a spline
221 method. A land-cover map (project SIOSE2005, <http://www.siose.es/>) was used as auxiliary data to identify
222 natural or rainfed areas and the main irrigated cropping systems (dominated by citrus and seasonal crop
223 systems). Evapotranspiration and crop coefficients were obtained from the NDVI (extracted from the
224 MODIS MOD13Q1 product – collection 6, tile h17v05; average values over 16 days; Villalobos et al.,
225 2006). Soil properties, including soil (root) depth, field capacity and wilting point are heterogeneous in the
226 surface water model. In particular, the spatial distributions of field capacity (3 atm on average) and wilting
227 point (15 atm on average) were computed using pedotransfer functions accounting for both soil texture and

228 organic matter contents identified in the LUCDEME project (Perez-Cutillas, 2013). More details on the
229 procedure can be found in Contreras et al., 2014, 2017).

230

231 The geometric definition of the Campo de Cartagena Quaternary aquifer (1119 km²), and its continuity
232 below the Mar Menor lagoon (135 km²), builds upon the 3D geological model proposed by Jiménez-
233 Martínez et al. (2012), in which a spatial resolution based on 500 × 500 m cells was adopted. The Quaternary
234 aquifer is made of sand, silt, clay and conglomerates and has an average thickness of 50 m, increasing from
235 west to east and reaching ~150 m near the lagoon. The aquitard below is made of very low conductive marls
236 and evaporates of the Pliocene with an average thickness of 60 m. This unit and the deeper confined aquifers
237 are not modelled, due to the negligible natural fluxes (i.e., those caused by raw vertical hydraulic gradient)
238 from the top Quaternary to the subjacent Pliocene and Messinian aquifers at the regional scale (Jiménez-
239 Martínez et al., 2011; García-Aróstegui et al., 2017).

240

241 The horizontal discretization of the 3D model was carried out with finite elements of irregular size, with
242 local refinements near zones with high topographic gradient (i.e., honouring the surface hydrology
243 network), along the coastline and near the current network of drains (Figure 2b). The vertical discretization
244 consists of 10 layers of elements, whose vertical size depends on aquifer thickness. Overall, the 3D mesh
245 contains 8 million hexahedral and prismatic finite elements (Figure 2c). Initial conditions are, as is often
246 the case in practice, highly uncertain. In order to minimize their impact, we model a long time period of 16
247 years (October 2000 to December 2016) that covers a wide range of hydrometeorological conditions.
248 Particularly relevant to this study are the identified hydrometeorological average (April 2002–March 2004),
249 wet (September 2008–August 2010) and dry periods (September 2013–August 2015). The impact of the
250 initial conditions on model results was evaluated by simulating the 16-year period using different starting
251 situations, showing that the results after December 2000 are independent of the chosen initial condition.
252 The model boundary conditions of the groundwater model are as follows:

- 253 (1) The western boundary coincides with a surface water divide. It is assumed that the underground water
254 divide approximately follows that contour and, correspondingly, an impervious boundary is assigned.
255 The impact of this assumption on the discharge of groundwater is negligible due to the large extent of
256 the model in the direction west to east (~43 km).
- 257 (2) The northern and southern boundaries of the model are the limits of the Quaternary aquifer. An
258 impervious boundary condition is assigned. Thus, it is assumed that the lateral contributions from or to
259 other aquifers (especially along the northern boundary) are negligible compared to recharge and
260 discharge.
- 261 (3) The eastern boundary is the lagoon, the volume of which is explicitly modelled. Nodes defining the
262 lagoon are attributed with a constant head boundary condition (0 m of equivalent fresh water level) and
263 a relative salt concentration of 37 kg/m³ (0 kg/m³ for nodes inland). Tides are not considered in the
264 model, since the lagoon regime is microtidal, with tidal range smaller than 0.6 m (maximum
265 astronomical tidal range in open sea in the vicinity, Sánchez-Badorrey and Jalón-Rojas, 2015). Such
266 fluctuations may cause local spatiotemporal perturbations of the hydraulic regime near the coastline.
267 However, their impact on groundwater levels is dampened by the temporal discretization of the model
268 (i.e., day-long intervals).
- 269 (4) The existing intra-basin water transfer Tajo-Segura and Taibilla channels, for agricultural and drinking
270 water supply purposes, respectively, are relatively modern (1979 and 1946, respectively) and under
271 continuous inspection. Thus, water losses from these infrastructures are negligible and ignored as water
272 sources for the aquifer.
- 273 (5) The six existing drains (Figure 2a) with corresponding temporal series of pumping rates are modelled
274 individually by means of distributed prescribed flow boundary conditions. The overall pumping is, on
275 average, <0.7 hm³/yr. The existing drains perform as constant head boundaries. To mimic that effect,
276 their geometry is explicitly included in the model. Similarly, their hydraulic parameters are estimated
277 separately.

278 (6) Active and abandoned pumping wells cannot be explicitly modelled due to lack of information (i.e.,
279 unknown location or history of pumped volumes). Notably, ~500 deep abandoned and poorly
280 constructed wells (>150 m depth) are distributed over the model domain, with higher density near the
281 coastline (Jiménez-Martínez et al., 2011). Such potentially leaky wells communicate the shallow
282 aquifer with the deep aquifers. The total volume of water transferred by leaky wells or pumped from
283 active groundwater wells was estimated by hydrochemical balance to be approximately 30–40% of the
284 overall recharge (Jiménez-Martínez et al., 2011). This large volume of groundwater does not reach the
285 lagoon and therefore, has a major impact on the volume of discharge, on the storativity of the system
286 or on both. Unfortunately, these “losses” (in the sense of aquifer sinks) cannot be accounted for directly
287 in the model as either point or diffuse sink boundary conditions because neither the coordinates of most
288 abandoned and active boreholes nor their distribution over the aquifer are known. The impact of
289 ignoring these losses on model results is further discussed below.

290

291 As a result of the aforementioned boundary conditions and model simplifications, the groundwater model
292 is a bucket model, in which the only source term is the recharge calculated by SPHY and the sink terms are
293 the discharge to the lagoon and the pumping from existing drains. Since losses caused by localized pumping
294 and vertical fluxes along leaky wells cannot be accounted for, model results in terms of discharge of
295 groundwater and nutrients must be taken as upper bounds. The spatial distribution and dose of the chemical
296 load (900–1600 kg/ha/yr, i.e., sum of ammonium nitrate NH_4NO_3 , phosphoric acid H_3PO_4 , potassium nitrate
297 KNO_3 , calcium nitrate $\text{Ca}(\text{NO}_3)_2$, ammonium phosphate $(\text{NH}_4)_3\text{PO}_4$, and magnesium nitrate
298 $\text{Mg}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$; Jiménez-Martínez et al., 2011) associated with agriculture is known. However, the uptake
299 efficiency of plants, and therefore the rate of percolation of those agrochemicals to the aquifer, is highly
300 uncertain and difficult to model in a simple manner. Concentration data near the coastline are available at
301 six wells (Figure 3). Temporal series display a general increase of nitrate concentration mainly caused by
302 the intensification of agricultural activities (e.g., an increased irrigated surface). The lack of data precludes

303 the explicit modelling of the budget of nutrients. Instead, we focus on possibly the most active contributor
304 to eutrophication, nitrate, and calculate the mass rate discharged into the lagoon by multiplying the
305 discharge of groundwater by the nitrate concentration. To that end, the coastline is divided into six segments
306 that are each attributed the nitrate concentration at the closest monitored well. Thus, it is assumed that
307 nitrate does not degrade along the path from the monitored well to the coastline. This assumption is
308 supported by the oxic character of the unconfined Quaternary aquifer, which precludes the degradation of
309 nitrates (Jiménez-Martínez et al., 2011). In this line of arguments, the denitrification of the upper part of
310 the aquifer underlying coastal wetlands does not play either a major role in nitrate degradation because
311 aquifer thickness is large.

312

313 **2.4. Parameterization and available data**

314 The groundwater flow model is parameterized by two unknown spatial distributions (hydraulic conductivity
315 K [m/d] and specific yield S_y [-], the latter being similar to the aquifer's effective porosity). These
316 parameters can be easily transformed into their 2D counterparts, i.e., transmissivity T [m²/d] and S [-] by
317 plugging in the aquifer saturated thickness b [m]: $T = Kb$ and $S = S_y + S_s b$, S_s being is the specific storage
318 [m⁻¹]. The low quality and scarcity of parameter data, e.g., arising from the prior analytical interpretation
319 of a few pumping tests (Tragsatec, 2013), precludes the estimation of model parameters on a cell-by-cell
320 basis. In addition, the such fine model discretization would make this computational problem unresolvable
321 in a reasonable amount of time. To overcome this problem, we first assume that model parameters are
322 homogeneous in the vertical direction. This allows us to display the model parameterization in in 2D by
323 plotting hydraulic diffusivity D [m²/d] = T/S . The hypothesis of vertical homogeneity is supported by the
324 pseudo-homogeneity observed in available stratigraphic sequences from exploration boreholes in the area
325 (Jiménez-Martínez et al., 2012). In contrast, K (especially) and S_y may vary several orders of magnitude
326 over small horizontal distances in Quaternary aquifers. To mimic this pattern, K and S_y are considered
327 heterogeneous and interpolated from values at 72 points distributed over the model domain (so-called pilot
328 points). Artificial drains are assumed to be homogeneous with individual parameterization (overall, 6

329 additional pilot points, one per existing drain). The value of K and S_y at pilot points is estimated via the
330 Regularized Pilot Points Method (RPPM, Alcolea et al., 2006), as implemented in PEST (Doherty, 2016),
331 a general-purpose maximum likelihood estimation software. Parameter calibration requires head data at
332 available boreholes in the area. Unfortunately, heads were measured only after drilling in most cases.
333 Overall, heads were measured more than once at 25 wells only, and long measurement records are available
334 at only 16 of them. Calibration was performed with head data at these 16 boreholes only (overall, 822 head
335 measurements). Remaining measurements (88) were used for model validation. The estimates of model
336 parameters reported in Tragsatec (2013) are included in the model as prior information. The reported
337 storativity values are highly uncertain and attributed a very low weight in the calibration, because the vast
338 majority of hydraulic tests were carried out in a single well (Meier et al., 1999).

339

340 **2.5. Management scenarios**

341 The model setup described so far is used to represent the current state of the system. The calibrated model
342 was then used to simulate three scenarios representing plausible management strategies aimed at reducing
343 the discharge of groundwater and nutrients into the Mar Menor lagoon. These scenarios, which consider
344 different pumping patterns and volumes, were devised in close consultation with the local authorities and
345 are therefore feasible in the near future. They were devised bearing in mind that (1) the expansion of the
346 irrigated area is not allowed by law, and (2) the overall goal is to reduce the release of agrochemical by-
347 products into the coastal lagoon. The model forecasts must be considered from a qualitative point of view
348 only, since the socio-economic evolution of the region and the impact of climate change (i.e., variations in
349 recharge) are not considered in the analysis. Nevertheless, the suggested scenarios are well suited to
350 environmental decision-making.

351

352 *Scenario 1.* The first scenario involves the increase of the pumping capacity of the six existing drains that
353 run parallel to the coastline in the southern sector (e.g., by enlarging the current cross section or by replacing

354 clogged filters). The existing drains have been operative since the end of 2008, and have a total length of
355 14.8 km. During the operational period 2008–2016, a mean annual rate of 0.7 hm³/yr of brackish
356 groundwater was pumped, which means a pumping rate capacity of 0.05 hm³/km/yr. In this scenario, the
357 current pumping capacity is multiplied by a defined pumping intensification factor α .

358
359 *Scenario 2.* The second scenario involves the existing drains and the construction of a set of new drains
360 with (1) a total length 6.6 km to the north of the Rambla del Albuñón (Figure 4) and (2) the design
361 characteristics of the existing drains (i.e., the same pumping rate capacity is assumed). The trace of the
362 proposed new drains accounts for urban areas, topography and current groundwater levels. For instance,
363 the maximum depth of the new drains was set to 6 m, which makes its implementation feasible and not
364 costly. Assuming the same pumping rate capacity as the existing drains, this scenario accounts for a total
365 pumping of 1 hm³/yr. As in scenario 1, a pumping intensification factor α is used to evaluate the impact of
366 a more intense pumping strategy on the discharge of groundwater and nutrients into the lagoon.

367
368 Scenarios 1 and 2 are described here as *localized scenarios* because pumping takes place along localized
369 linear infrastructures. In both cases, the high salt and nitrate content of the pumped groundwater must be
370 removed prior to its use for irrigation purposes (as it is done nowadays in the southern sector). This would
371 include the construction of new treatment facilities and/or the conduction of the pumped water to the
372 existing ones. The management of sub-products such as rejected brackish water would also need to be
373 included in an integral management plan, which is far beyond the scope of this paper.

374
375 *Scenario 3.* The third scenario, described here as a *distributed scenario*, envisions the pumping of
376 groundwater at the many wells scattered over the irrigated area, which are coupled with private
377 desalination plants. The pumping from the current drains is included, but not the construction of the new
378 drains suggested in scenario 2. The water demand for agricultural purposes in the T-S WT irrigation sectors
379 (shaded area in Figure 4) is on average 76 hm³/yr and is mostly supplied by the T-S WT (on average 61

380 hm^3/yr , but highly variable with a maximum value of $132 \text{ hm}^3/\text{yr}$ in 2014; Jiménez-Martínez et al., 2016).
381 The remaining water demand is covered by groundwater pumped from the deep confined aquifers (on
382 average $15 \text{ hm}^3/\text{yr}$), whose quality for irrigation purposes is better than that pumped from the Quaternary
383 shallow aquifer. The third scenario suggests pumping from the shallow aquifer instead, which would reduce
384 the discharge of polluted groundwater into the lagoon and, in addition, preserve the confined aquifers. The
385 spatial pumping pattern assumed in this scenario follows that of groundwater use per irrigation sector
386 described in Hunink et al. (2015). As for the *localized scenarios*, the necessary additional infrastructure for
387 the desalination/denitrification of brackish water is not considered here.

388

389 **3. Results**

390 **3.1. Model performance and parameterization**

391 The performance of the calibrated model is evaluated both in terms of goodness of fit to available hydraulic
392 head measurements and plausibility of the calibrated model parameters. Figure 5 shows a scatter plot of the
393 measured and calculated heads after the calibration and validation exercises, and the histogram of residuals
394 (calculated minus measured value) after calibration. The Root Mean Square Error (RMSE) is 1.3 and 4.3
395 m for calibration and validation, respectively, while the corresponding Maximum Absolute Errors (MAE)
396 are 4.3 and 14.6 m. The model tends to slightly overestimate heads at some points (Figure 5a), which leads
397 to a right tail in the residuals (Figure 5b). This was expected because head measurements at a few points
398 were collected during pumping. Unfortunately, the corresponding dates of pumping are not reported and
399 those measurements cannot be filtered. An additional contribution to the positive misfit is the proximity of
400 some monitored wells to active pumping wells, which cause a drawdown that is captured in the
401 measurements but not by the model (i.e., because the location of pumping wells and/or the pumping rates
402 are unknown). Nonetheless, both calibration and validation fits are acceptable, with mean residuals of 0.27
403 and 1.29 m respectively. Fits to available data at selected observation points are presented in section 3.2.

404

405 Model parameters K and S_y are presented in terms of hydraulic diffusivity in Figure 6a. Note that hydraulic
406 parameters of existing drains were estimated separately and are not reported in Figure 6a because the mean
407 estimated diffusivity at drains is $\sim 500 \text{ m}^2/\text{d}$, which would distort the colour bar. This very high value stems
408 from their high hydraulic conductivity and very low storativity. Figure 6b shows the posterior parameter
409 uncertainty, as measured by the posterior standard deviation of model parameters σ . The 95% confidence
410 interval of a given model parameter p is calculated on a log scale as $\log_{10} p \pm 2\sigma$. Thus, small values of σ
411 are translated into low uncertainty of the estimated parameters. The largest σ values are found near the La
412 Unión mining district (in the south), where no head data are available, and near the mouth of the Rambla
413 del Albuñón (on the western-most point on the lagoon). The latter received the rejected by-product of
414 desalination plants, thus behaving sporadically like a river that infiltrates brackish water. The leakage of
415 the surface drainage network is not considered in the model because of lack of information. However,
416 available head measurements in the vicinity are affected by the river-groundwater seepage connection.
417 Thus, it is not unexpected that the calibration process, in an attempt to fit head data that cannot be fitted
418 with current boundary conditions, suffers from some instability that inflates the posterior standard
419 deviation. Overall, posterior standard deviations are small and far below 1. This means that the lower and
420 upper bounds of the confidence interval of an estimated parameter are always within the same order of
421 magnitude.

422

423 **3.2. Evolution towards the current state**

424 The calibrated model allows evaluation of the current state of the aquifer, the different components of the
425 water balance and their relationships. Recharge and discharge are the main mechanisms driving the
426 hydrodynamic system and are modelled explicitly. As described above, vertical losses from the shallow to
427 deeper aquifers and pumping wells are not modelled due to lack of information. Thus, the discharge rates
428 of groundwater and nitrate presented in this section are upper bounds and correspond to the most pessimistic
429 situation from an ecological point of view.

430

431 Recharge varies greatly from one day to the next and also exhibits marked seasonal and yearly trends, which
432 cause fluctuations in discharge, partly dampened by the aquifer. Although technologically sounding and
433 with high irrigation efficiency, agricultural practices cause sometimes peaks in the temporal distribution of
434 recharge. Such peaks are favoured by (1) the shallow topographic gradient towards the east, which hinders
435 surface run-off, and (2) the combination of the rainfall characteristic of semi-arid regions (i.e., unevenly
436 distributed into a few intensive events highly variable in space and time) and the high water content of the
437 soil caused by the permanent agricultural activity, which increases relative hydraulic conductivity, thus
438 favouring recharge (Jiménez-Martínez, 2010).

439

440 Figure 7a shows the estimated mean annual recharge for the studied period 2000–2016. The mean annual
441 recharge is ~73 mm/yr, but higher values of ~300 mm/yr are found in the southeast irrigated area. These
442 values are consistent with the results of in situ studies that took into account the most representative crops
443 and agricultural practices in the region, i.e., rotation of lettuce and melon, artichoke, and citrus, all of them
444 under drip irrigation (Jiménez-Martínez et al., 2010). Figure 7b shows the monthly averaged water mass
445 balance components for the study period (2000-2016), i.e., precipitation and irrigation as inflows, and actual
446 evapotranspiration, surface runoff, interception and recharge as outflows. Figure 8 shows the contours of
447 hydraulic heads calculated with the calibrated model for the considered average hydrometeorological period
448 April 2002–March 2004. The hydraulic gradient increases from west to east. The increase is highly non-
449 linear and very rapid in the vicinity of the coastline. The overall distribution of hydraulic heads does not
450 vary greatly in time. In fact, the head fluctuation during dry and wet periods (around mean values during
451 the average period) is only -0.5 and 2 m, respectively. The temporal evolution of hydraulic heads at selected
452 points is also shown in Figure 8. Several observations are apparent in these plots: (1) a decreasing trend of
453 heads with time, directly related to the proliferation of small private desalinization plants (i.e., a situation
454 similar to that suggested by the distributed scenario), (2) a partial recovery of groundwater levels during
455 the wet period (September 2008–August 2010), and (3) the strong reaction of the aquifer to episodic peaks

456 in recharge. Finally, the maximum penetration of the saltwater wedge (i.e., the toe, green line in Figure 8)
457 for the average period is <330 m. The penetration of the toe during dry and wet periods is very similar
458 (shifts of a few tens of meters with respect to the toe during the average period) and the fluctuation is not
459 reported in Figure 8.

460

461 The calibrated model was used to quantify the spatio-temporal distribution of groundwater and nitrate
462 discharge into the lagoon (Figure 9). The perimeter of the lagoon was divided into 15 segments of length
463 ~2 km, taking as starting point the mouth of the Rambla del Albujón. For each segment, the fluxes of
464 groundwater at the corresponding nodes are integrated daily, which yields the total daily discharge of
465 groundwater along the segment. The discharge of nitrates is calculated by multiplying the daily discharge
466 of groundwater by nitrate concentration at the closest monitored borehole in Figure 3. The discharge occurs
467 mainly in the central sector of the lagoon (66–70% of groundwater discharge and 71–75% of nitrate
468 discharge occurs along segments North2 to South2, depending on the hydrometeorological period) and
469 diminishes almost monotonically when moving northwards or southwards. The discharge across segments
470 to the north of the Rambla del Albujón (North1 to North7; 60–62% of total groundwater discharge and 55–
471 58% of total nitrate discharge) is slightly larger than that across southern segments. This is a direct
472 consequence of the pumping from existing drains in the southern part.

473

474 The potential daily discharge of groundwater and nitrate load into the lagoon is shown in Figure 10. These
475 correspond to the sum of the curves presented in Figure 9. Five different periods are apparent:

476 - From 2000 to 2005, the discharge of groundwater oscillates seasonally around a mean value ~0.19
477 hm³/d. Strong peaks in the calculated hydrogram are observed in response to peaks in the recharge
478 record corresponding to episodic intense rain events. The discharge of nitrates fluctuates in similar
479 way, around a mean value of ~22,000 kg/d.

- 480 - From 2005 to 2009, the discharge of groundwater maintains the same seasonal trend, but the
481 discharge of nitrates increases progressively to ~27,000 kg/d. This is a result of the progressive
482 increase of nitrate concentration in the aquifer (Figure 3).
- 483 - From 2009 to 2011, recharge increases substantially (i.e., a wet period), which leads to an increase
484 of the discharge of both groundwater and nitrates, reaching mean stable values of ~0.2 hm³/d and
485 a plateau ~34,000 kg/d, respectively.
- 486 - From 2011 to 2014, recharge and, correspondingly, discharge of groundwater diminish
487 substantially in response to a sequence of mid to dry hydrological years. However, the discharge
488 of nitrates into the lagoon remains stable (and maximum) at ~34,000 kg/d. This is explained by the
489 continued increase of nitrate concentration in the aquifer (Figure 3).
- 490 - From 2014 to 2016, the discharge of groundwater continues to diminish, following the trend of the
491 previous period. The discharge of nitrate also diminishes, but more rapidly. This trend is likely a
492 consequence of the introduction of technical improvements in irrigation systems, and represents a
493 hopeful step for the sustainable development of the region and the survival of the Mar Menor
494 ecosystem. The largest rainfall event took place at the end of the simulation period (December
495 2016), which precludes the evaluation of its impact on discharge.

496

497 Table 1 summarizes the components of the water balance during wet, average and dry periods, the mean
498 for the studied period, and the corresponding nitrate loads released into the lagoon. Reported values
499 correspond to averaged model outputs. There are large differences in recharge during the three characteristic
500 periods. However, the maximum discharge of groundwater into the lagoon (i.e., in the sense of potential,
501 ignoring vertical fluxes to deeper aquifers and the pumping from groundwater wells) is relatively constant.
502 The water excess during wet periods is translated into an enhanced capacity of the aquifer that leads to an
503 overall increase of groundwater levels (recall Figure 8). Nonetheless, such variation is small compared to
504 the average volume of groundwater in the aquifer (~2575 hm³ as evaluated by the model). On average, the
505 maximum discharge of nitrate into the lagoon is relatively similar during the dry and wet periods, but was

506 lower during the earlier average period, as discussed above. We attempted to address the impact of the
507 unconsidered sink terms by subtracting 30% and 40% of the overall recharge (Jiménez-Martínez et al.,
508 2011) from the mean discharge of groundwater (values in italics in Table 1). This reduces the discharge of
509 groundwater by a factor 1.5 to 1.75, assuming that the losses do not have an impact on aquifer storativity.
510 This factor is larger (1.9 to 2.3) considering the discharge of nitrates into the lagoon. The large disparities
511 between maximum (i.e., as calculated) and possible discharge values highlight the need for newly acquired
512 measurements to reduce model uncertainties, mainly caused by lack of information.

513

514 **3.3. Analysis of integrated management scenarios**

515 *Localized scenarios.* A simulation of the whole 16 years period was performed. Only the dry and wet
516 hydrometeorological periods were analysed because the existing drains are operative since end of 2008
517 (i.e., not during the average hydrometeorological period). Figure 11a shows the reduction in the discharge
518 of groundwater into the coastal lagoon as a function of pumping rate with either existing or existing together
519 with extended drains. These localized scenarios are not capable of inverting the current flow regime (aquifer
520 to lagoon, positive values of discharge in Figure 11a) during a wet period (blue curves), even if the pumping
521 rate at drains is increased 150-fold with the current or extended drains. The flow regime is inverted during
522 a dry period if the pumping capacity is increased by a factor of 80 (with current drains only) and 60 (current
523 plus extended drains). Figure 11b shows the reduction in discharge in terms of mass flux of nitrate into the
524 lagoon. Both scenarios reduce the discharge of nitrates, particularly the second scenario with extended
525 drains. The reduction in nitrate discharge increases with pumping intensification and is especially large
526 during dry periods. Note that, in this case, the discharge of nitrates is again the maximum possible (i.e., the
527 potential discharge) because sink terms are ignored by the model. As such, the discharge rates presented in
528 Figure 11 must be considered as the most pessimistic situation from an ecological point of view.

529

530 *Distributed scenario.* The distributed pumping of $\sim 15 \text{ hm}^3/\text{yr}$ from the shallow unconfined Quaternary
531 aquifer (only from the sectors irrigated with water from the T-S WT; shaded area in Figure 4) causes a
532 small reduction in the groundwater discharge into the Mar Menor lagoon during the simulated wet and dry
533 periods (points in Figure 11a). This is equivalent to the reduction caused by a 3–5 times greater pumping
534 rate in the localized scenarios (for dry and wet conditions, respectively). An even greater reduction in the
535 discharge of nitrates is observed (Figure 11b). A maximum reduction of $\sim 2000 \text{ kg/d}$ is observed during
536 both dry and wet periods, which corresponds to a high pumping rate (from 10 to 100 times the current one)
537 under the localized scenarios.

538
539 The intersections between the curves in Figure 11a and the horizontal dashed line (0 discharge) represent
540 an old envisaged management strategy known by local stakeholders and policy-makers as “zero spill”
541 (referring to zero spill of nutrients, an unfortunate and misleading term supposed to mean “zero discharge”).
542 A zero discharge of groundwater into the lagoon could be achieved during dry periods with pumping
543 intensification factors of 82.5 and 57.5 for scenarios 1 and 2, respectively, and would require even higher
544 values during wet periods. The volumes of pumped groundwater corresponding to such high intensification
545 factors would be 57.8 and 60.4 hm^3/yr for the scenarios 1 (current drains) and 2 (current plus extended
546 drains), respectively. Such volumes are far from being physically plausible. In addition, a null mean
547 discharge (along the whole perimeter of the Mar Menor) does not necessarily imply a null discharge of
548 nutrients. A zero mean discharge of groundwater means that the volume of brackish water pumped from
549 drains is equivalent to the discharge of groundwater along areas not affected by drains, where nitrate
550 discharge would still take place. Moreover, shallow drains have a certain catchment zone and cannot capture
551 the nitrates all along the saturated thickness of the unconfined aquifer ($\sim 100 \text{ m}$ in the area affected by
552 drains). Thus, nitrate discharge may also take place at the area affected by drains. Consequently, although
553 the drains would capture larger masses of nitrates, a “zero spill” of nutrients into the Mar Menor is, at best,

554 utopic. None the less, the simulation of this “old-fashion” management strategy has been included in Figure
555 11 for completeness only.

556

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559

560

561 **4. Discussion**

562 This section discusses the main strengths and weaknesses of the model and the proposed management
563 scenarios. We start by discussing the main weakness of our work, i.e., that the underlying conceptual model
564 is unquestionably wrong (but forced by the lack of information; Shapiro, 2007). The pumping from
565 groundwater wells and the vertical fluxes from the shallow Quaternary aquifer to the deeper confined
566 aquifers through leaky wells have been ignored because information, hard or soft, is not available to model
567 them explicitly. Instead, we approximated this by applying an overall reduction in the discharge of
568 groundwater into the lagoon (30–40% of the overall recharge, i.e., 26–35 hm³/yr). We argue that the low
569 quality of groundwater from the Quaternary aquifer (electric conductivity ~5000 μS/cm and >100 mg/L
570 NO₃⁻) precludes its use for irrigation or any other consumptive use (only 2 hm³/yr according to ITGE, 1991).
571 This small value partly reduces the consequences of our “forced” hypothesis. In contrast, vertical losses to
572 deeper aquifers may be important. However, we argue that this is not the case in the Campo de Cartagena
573 plain. Distributing 26–35 hm³/yr uniformly among 500 leaky wells (Jiménez-Martínez et al., 2016) yields
574 an individual loss of 1.7–2.2 L/s. Tragsatec (2013) and Contreras et al. (2017) report reference
575 transmissivity values of up to 1600 m²/d at zones where aquifer saturated thickness was small (in the range
576 1–10 m, the average being 50 m). As such, even larger transmissivity values can be expected and are
577 actually revealed by the model. Plugging the individual loss rates and this transmissivity value into Thiem’s
578 formula (Thiem, 1906) suggests a distributed steady state drawdown ~10–14 cm. This range is comparable

579 with the measurement errors (e.g., in the reference elevation of the wells, in the manual collection of head
580 data) and should not alter the hydrodynamic regime in the aquifer, especially because losses are small point
581 sinks in the aquifer that, moreover, are well distributed in space. A second back-of-the-envelope calculation
582 also supports our argument. If a porosity $\phi = 0.15$ is assumed (Contreras et al., 2017), the drop in
583 groundwater levels caused by leaky wells is <15–20 cm (by simply distributing losses uniformly over the
584 1119 km² aquifer), which is very low compared to the head fluctuations caused by recharge or by the
585 pumping from existing drains. In fact, the total volume of groundwater stored in the aquifer is ~2575 hm³
586 (Contreras et al., 2017). Thus, the unconsidered “lost” volume represents 1–1.3% of the total volume of
587 groundwater in the aquifer. In view of these arguments, the available head measurements are unlikely to be
588 perturbed by local losses to underlying aquifers. Thus, the estimated model parameters are unlikely to be
589 affected by the hypothesis of ignoring leaky and active wells.

590

591 The model was calibrated to available measurements in the period October 2000–December 2016. An upper
592 bound of mean groundwater discharge into the lagoon, i.e., in the absence of the aforementioned losses, is
593 78 hm³/yr. Estimated losses of 26–35 hm³/yr caused by vertical fluxes and pumping are slightly lower (but
594 still in accordance) with those reported in previous work (38 hm³/yr by ITGE, 1991; 44.5 hm³/yr by
595 Domingo-Pinillos et al., 2018 and <46 hm³/yr by Jiménez-Martínez et al., 2016). The effective discharge
596 of groundwater into the Mar Menor lagoon assuming losses of 26–35 hm³/yr has been roughly estimated
597 by mass balance in the range 45–53 hm³/yr (Table 1). This range is quite controversial. For example, ITGE
598 (1991) reported 5 hm³/yr only, presenting a back-of-the-envelope calculation using a constant head gradient
599 and a homogeneous transmissivity. A similar value (6.2 hm³/yr) has been recently reported in the
600 Hydrological Plan of the Segura Basin 2015-2021
601 (<https://www.chsegura.es/chs/planificacionydma/planificacion15-21/>), which simply updates the ITGE
602 estimation with revised pumping rates. More recently, Jiménez-Martínez et al. (2016) and Domingo-

603 Pinillos et al. (2018) report discharge values of 68 and 34.8 hm³/yr, respectively. These values are closer to
604 the range suggested by our model.

605
606 We estimated nitrate discharge by weighting the discharge of groundwater with a spatial distribution of
607 nitrate concentration in the aquifer. On average, the aquifer discharged 10.2 Mkg/yr into the lagoon during
608 the studied period. This value is in good agreement with a previous evaluation of nitrate discharge of ~13.6
609 Mkg/yr caused by a groundwater discharge of 68 hm³/yr (García-Aróstegui et al., 2017). An average nitrate
610 discharge of 10.2 Mkg/yr may sound high, but is realistic given the dimensions of the diffuse source term
611 (i.e., the irrigated area, 477 km²) and the chemical load used in the intensive agriculture in the area (900–
612 1600 kg/ha/yr, Jiménez-Martínez et al., 2011) that lead to a total chemical input (mainly nitrate) of ~27–48
613 Mkg/yr. A second input of nitrate into the lagoon, not considered in this study, is surface water. For
614 example, Velasco et al. (2005) evaluated the surface discharge of nitrate at the mouth of the Rambla del
615 Albujión after the stormy period September 2002–October 2003 as 2 Mkg/yr. Bearing in mind that this
616 number summarizes a point discharge, a diffuse discharge of 10.2 Mkg/yr along a 30.3 km long coastline
617 cannot be viewed as an unrealistically high value. Ignoring water renewal, the degradation of nitrate and its
618 retention in the lacustrine sediments, a maximum nitrate concentration in the lagoon of ~7.5 mg/L can be
619 estimated. This upper bound is, indeed, larger than the measured nitrate concentrations (1 mg/L in the centre
620 of the lagoon, but 3.7 mg/L near the coast; Baudron et al., 2015; Velasco et al, 2005; DGA-MAGRAMA,
621 2018), but still in good agreement.

622
623 Despite the inherent uncertainties associated with any model (especially the first version of a novel model),
624 the reconstruction of the aquifer hydrodynamics towards the current state allows an explanation of the
625 recent algal blooms observed in the coastal lagoon. The large peak in nitrate concentration following a
626 severe storm (the strongest in 16 years) is clearly observable in Figure 10. This almost immediate response
627 of the aquifer can be easily explained by observing its history. Algal blooms did not occur in the period

628 2000–2008, when nitrate discharge into the lagoon was in the order of 25,000 kg/d or below. However, the
629 exceptionally wet period (end 2008–mid 2010) along with the permanent increase of nitrate concentration
630 in the aquifer (Figure 3) resulted in a rise and posterior stabilization of discharge of nitrates into the lagoon
631 with rate ~34,000 kg/d (end 2009–end 2013). Although discharge of both groundwater and nutrients have
632 showed decreasing trends in recent years, a high load of nutrients in the aquifer has been reached nowadays.
633 Since mid 2015, intense rainfall storm events like those at the end of December 2016 trigger high pulses of
634 nutrient inputs into the lagoon, with consequent anoxic conditions and algal bloom episodes that cause
635 death of the lagoon’s biota (see e.g., DGA-MAGRAMA, 2018). The values of nitrate discharge presented
636 in this paper are upper bounds due to the many factors controlling the discharge of nutrients into the lagoon
637 that have been disregarded, e.g., (1) denitrification and phosphorus retention of the upper part of the aquifer
638 underlying the wetlands along the coastline (Velasco et al., 2006; Tercero et al., 2017), (2) temperature
639 fluctuations in the aquifer, and (3) connectivity with the Mediterranean Sea that controls water renewal in
640 the lagoon. The contribution of the surface drainage network has also been ignored, e.g., (1) acid drainage
641 from the abandoned Cartagena-La Unión mining district, (2) spills of urban effluents (especially during and
642 shortly after intense rainfall events, Velasco et al., 2005) that contribute nitrates together with other
643 nutrients such as additional phosphates, and (3) the flush of nitrates in the surface (Esteve Selma et al.,
644 2016).

645
646 Our numerical model helps to understand the past and to know the present of the Campo de Cartagena
647 plain–Mar Menor coastal lagoon system, but also to forecast its future state. In this paper, three plausible
648 management scenarios aimed at reducing the nutrient load into the lagoon were explored. The localized
649 scenarios involving drains are efficient to reduce the discharge of groundwater into the lagoon, provided
650 that current or projected basic pumping rates at drains are substantially increased. In fact, only the scenario
651 that includes the construction of new drains and with very high pumping rates is able to reduce the nitrate
652 discharge below 25,000 kg/d. The drawback of the localized scenarios is the risk of seawater intrusion
653 (inversion of flow regime) during dry periods, which would increase the desalinization costs for irrigation

654 and cause other environmental problems. Instead, the distributed scenario, which could be considered as a
655 complementary strategy to the current pumping existing drains, would also satisfy the water requirements
656 of crops and reduce the dependency of water resources provided by the inter-basin T-S WT. Assuming a
657 distributed pumping rate of $\sim 15 \text{ hm}^3/\text{year}$, the reduction in the discharge of groundwater into the lagoon
658 would be still small. However, the reduction in the nitrate load into the lagoon would be considerable
659 ($\sim 2000 \text{ kg/d}$). Most likely, a combination of the localized and distributed scenarios is necessary to achieve
660 a sustainable regime of the Campo de Cartagena plain–Mar Menor coastal lagoon system.

661

662 **5. Concluding remarks**

663 The system Campo de Cartagena plain-Mar Menor coastal lagoon is a characteristic example of a highly-
664 modified and anthropized hydro-ecosystem. Multiple pressures and associated impacts on the lagoon are a
665 direct consequence of intensive exploitation of the landscape. The current significant ecological
666 deterioration of the lagoon makes it necessary and urgent to adopt integrated and sustainable management
667 strategies to alleviate pressures on the system, and to enhance the resilience of the region against future
668 scenarios of land use and climate change.

669

670 In spite of the considerable efforts over the last decades to improve the understanding of the interaction
671 between the Campo de Cartagena plain and the Mar Menor coastal lagoon, there was a major gap regarding
672 the underground connection, which has a considerable impact on both the vulnerability of the lagoon and
673 on the availability of groundwater resources inland. In this study, we have presented an integrated 3D
674 hydrogeological model that couples a surface hydrology model with a groundwater model. A reconstruction
675 over sixteen years (2000-2016) of the system hydrodynamics reveals clear-cut links between groundwater
676 inputs and observed algal blooms in the lagoon. The discharge of groundwater and nitrates presented in this
677 paper provides an upper bound for the actual amounts due to model limitations caused by lack of
678 information.

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The calibrated model was used to simulate mitigation alternatives aimed at reducing the discharge of nutrients into the lagoon to ensure its ecologic health. Three scenarios involving pumping from drains and distributed pumping have been proposed. All three are able to reduce the discharge of groundwater into the lagoon and, correspondingly, the discharge of nitrate, assumed to be one of the main responsables of algal blooms. Unfortunately, none is capable of maintaining the mass flux of nitrate below tolerable levels. Likely, a combination of pumping from drains (localized scenarios) and distributed pumping from inland wells (distributed scenario) would provide a viable solution. None the less, the spatio-temporal quantification of groundwater discharge presented in this paper is a valuable tool for the design of new management alternatives and their evaluation.

Despite the model is able to accurately reproduce the recent history of the aquifer, much remains to be done. Because of its novelty and early development stage, some uncertainties still remain unresolved and should be coped in upcoming exercises. Uncertainties mostly arise from (1) the scarcity of measurements available to model calibration (of both heads and model parameters), and (2) the lack of information about aquifer's sink terms, i.e., the vertical transfer of groundwater to deeper aquifers through leaky wells and localized groundwater pumping. Improvements to the model are expected to better narrow the range of discharge into the lagoon, and to accurately quantify the source of irrigation water and the interactions between shallow and deeper aquifers. Climate change scenarios, which clearly impact on the recharge patterns, or other management strategies, e.g. optimization of adaptive pumping along the coastline or surface water-groundwater conjunctive use, may also be simulated in upcoming exercises. The modelling exercise presented here must be viewed as a first and hopeful step in the direction of achieving a more integrated and holistic water management scheme for the sustainability of the Campo de Cartagena-Mar Menor lagoon agroecosystem.

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714

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905 **Tables**

906

907 **Table 1.** Mean values of the water balance components in the Quaternary aquifer, and nitrate load released
 908 into the lagoon for wet, average and dry hydrometeorological periods, and for the complete 16-year study
 909 period. All values are direct model outputs, except those italicized, which represent the estimated discharge
 910 of nitrate if the vertical fluxes to deeper aquifers and the pumping from the shallow aquifer (overall 30–
 911 40% of the recharge) are taken into account. The nitrate discharge in the presence of vertical fluxes and
 912 pumping were estimated using the mean NO₃⁻ concentration in monitored wells (dashed grey line in Figure
 913 3).

	Wet period (Sep. 2008–Aug. 2010)	Average period (Apr. 2002–Mar. 2004)	Dry period (Sep. 2013–Aug. 2015)	All periods (Oct. 2000–Dec. 2016)
Recharge (hm ³ /yr)	233.3	62.3	12.2	83.6
Discharge (hm ³ /yr)	84.9	80.9	69.5	78.3 <i>53.3^a – 44.9^b</i>
Drains (hm ³ /yr)	0.5	NA*	0.9	0.4
Storage variation (hm ³ /yr)	147.9	-18.6	-58.2	4.9
Nitrate discharge (Mkg/yr)	11.8	8.2	11.4	10.2 <i>6.9^a – 5.9^b</i>

*: Drains operational since 2008.

a, b: Values corresponding to vertical fluxes and pumping corresponding to 30% and 40% of the recharge, respectively.

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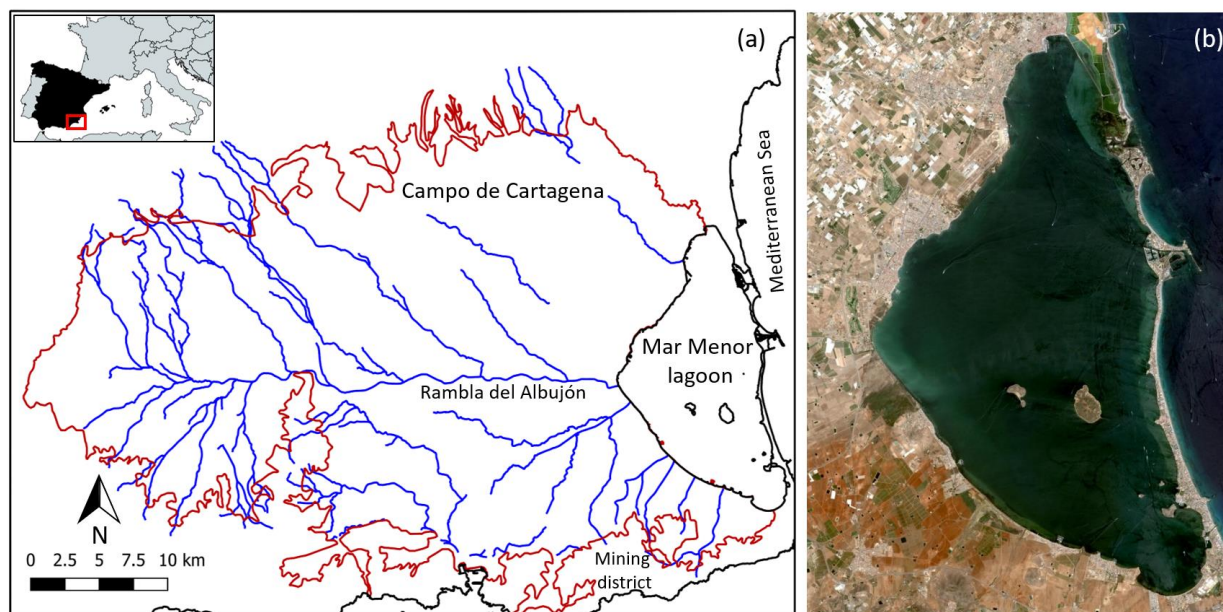
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919 **Figures**

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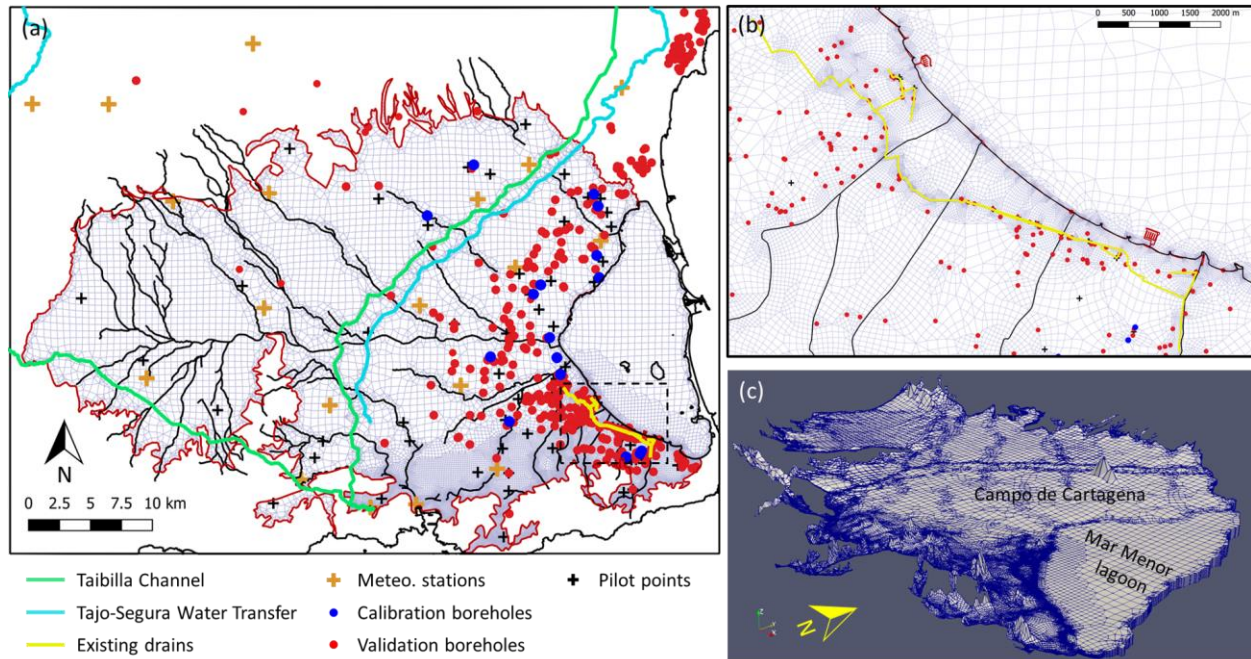


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922 **Figure 1:** (a) The hydrogeological system of the Campo de Cartagena plain-Mar Menor coastal lagoon.

923 The red line depicts the contour of the Quaternary aquifer (i.e., the limit of the groundwater flow
924 model). The blue lines depict the watercourses that define the surface drainage network. For its
925 relevance to this study, only the central watercourse “Rambla del Albujón” is labelled. The frame
926 encompasses the surface water flow model; (b) Aerial view of the Mar Menor lagoon.

927



928

929 **Figure 2:** (a) The model set-up, including the surface water network, existing water transfers and drains,

930 meteorological stations, observation boreholes for model calibration/validation and pilot points;

931 (b) Detail of the fine model discretization in the vicinity of existing drains; (c) 3D view of model

932 discretization (vertical exaggeration factor $\times 10$).

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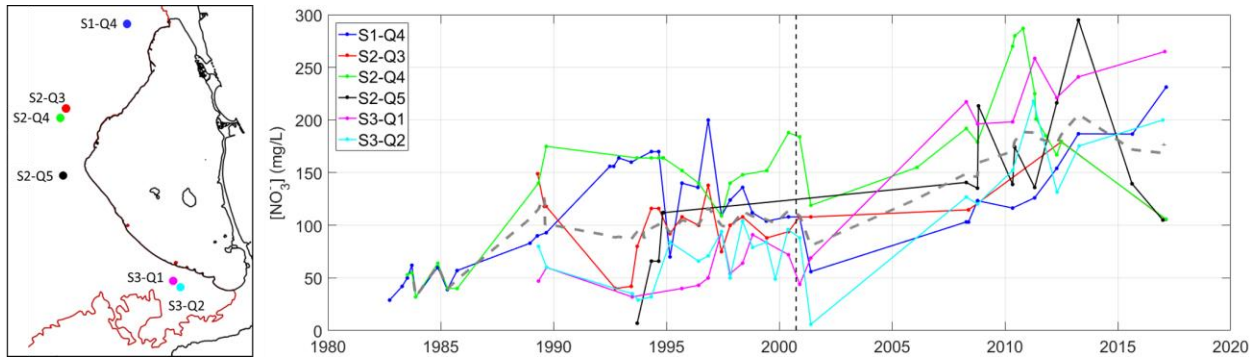
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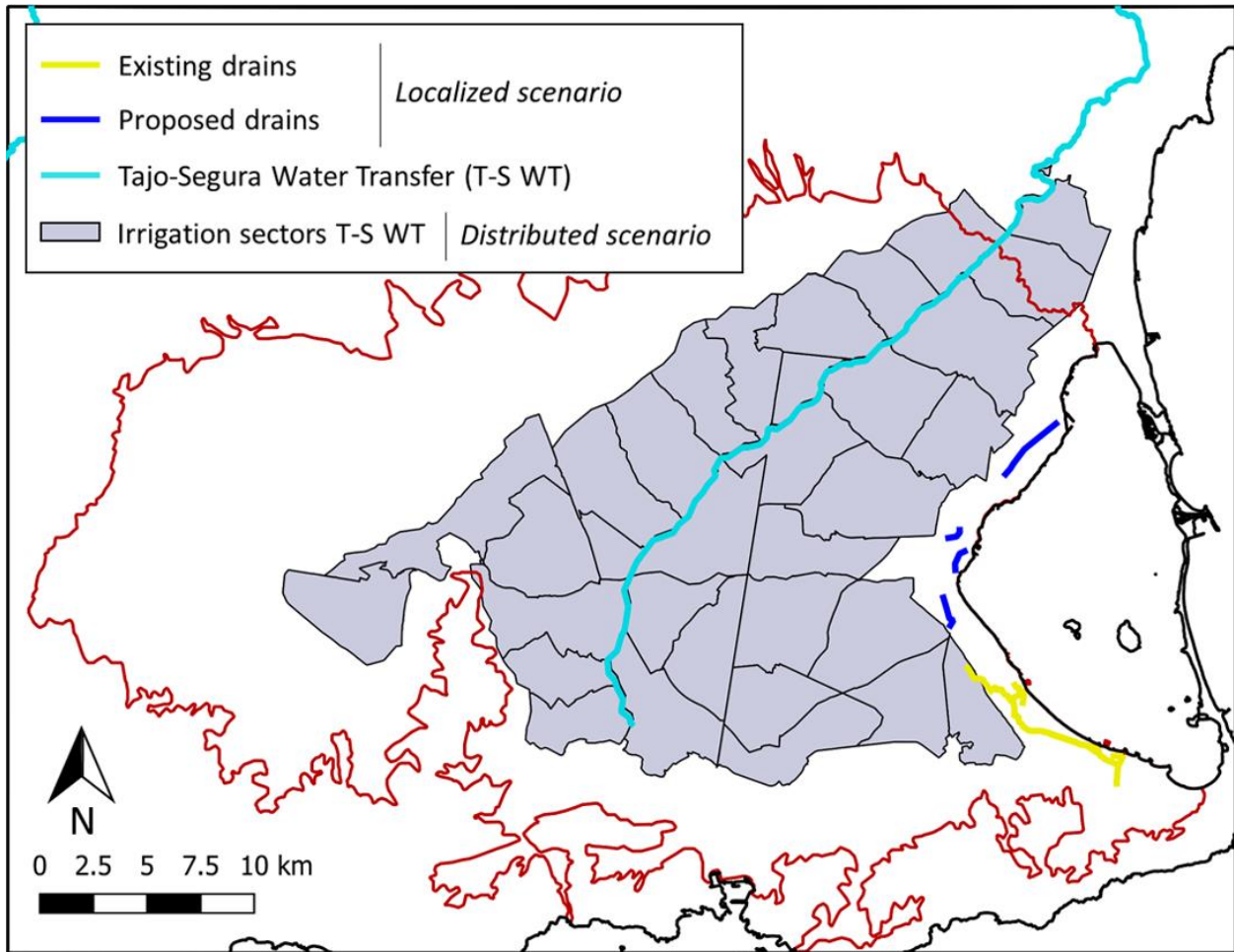


939

940 **Figure 3:** Location of wells where nitrate concentration is monitored (left) and the temporal evolution of
 941 nitrate concentration over the period 1980–2017 (right). The vertical dashed line depicts the
 942 beginning of the simulated period (October 2000). The grey dashed line depicts the mean
 943 concentration in monitored boreholes. Monitoring network: IGME-CHS.

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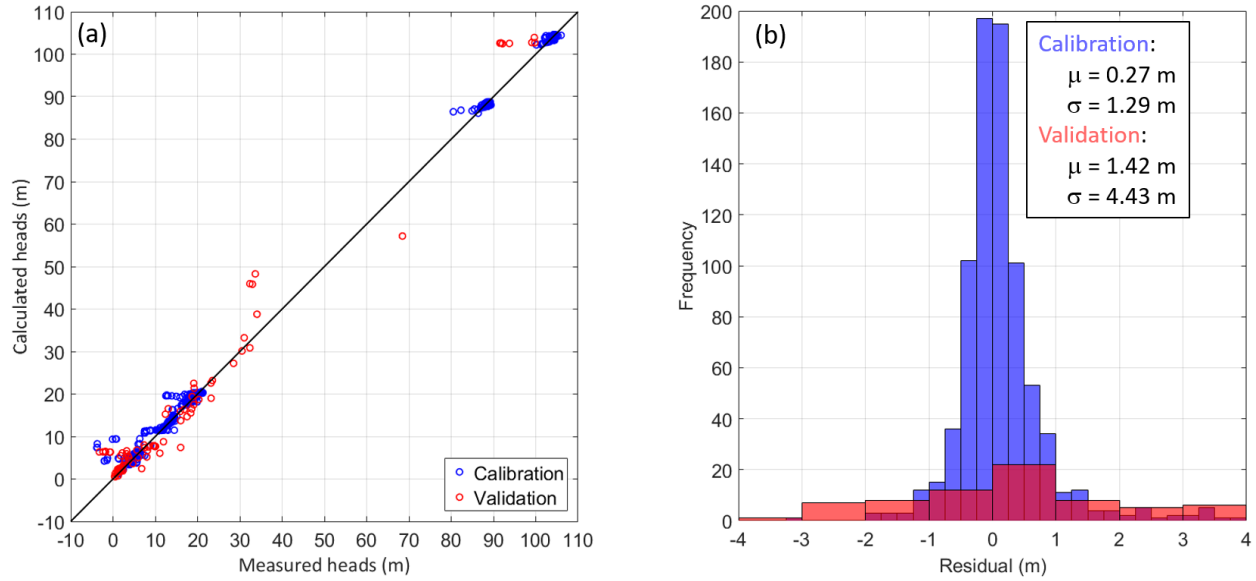


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947 **Figure 4:** Localized and distributed management scenarios.

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951 **Figure 5:** (a) Scatter plot of the measured and calculated hydraulic heads after the calibration (blue) and
 952 validation exercises (red); (b) Histograms of residuals, defined as calculated minus measured
 953 values. Note that fewer bins are used to define the histogram of residuals for the validation
 954 exercise due to the reduced number of measurements. The inset gives the mean residual μ and
 955 standard deviation σ of the distribution of residuals.

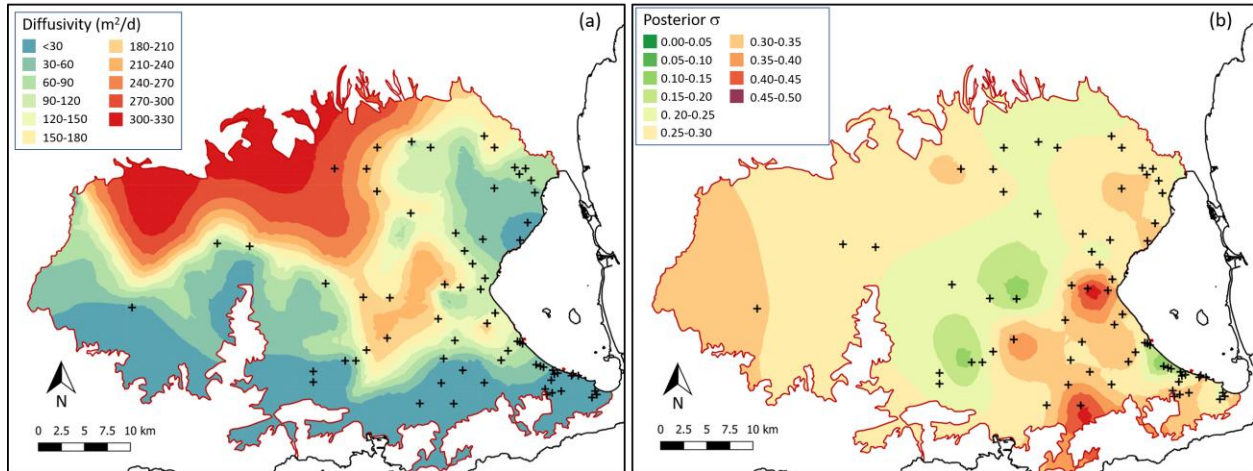
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962 **Figure 6:** (a) Spatial distribution of hydraulic diffusivity after calibration. The estimated mean diffusivity

963 of existing drains is $\sim 500 \text{ m}^2/\text{d}$ and is not displayed here to avoid distorting the colour scale. The

964 crosses depict the pilot points, where the estimation of model parameters is actually carried out.

965 Given the absence of information on model parameters in the lagoon, pilot points are located

966 inland only. Thus, estimated diffusivity values in the lagoon are highly uncertain and excluded

967 from this plot; (b) Composite of posterior standard deviations of the estimated parameters.

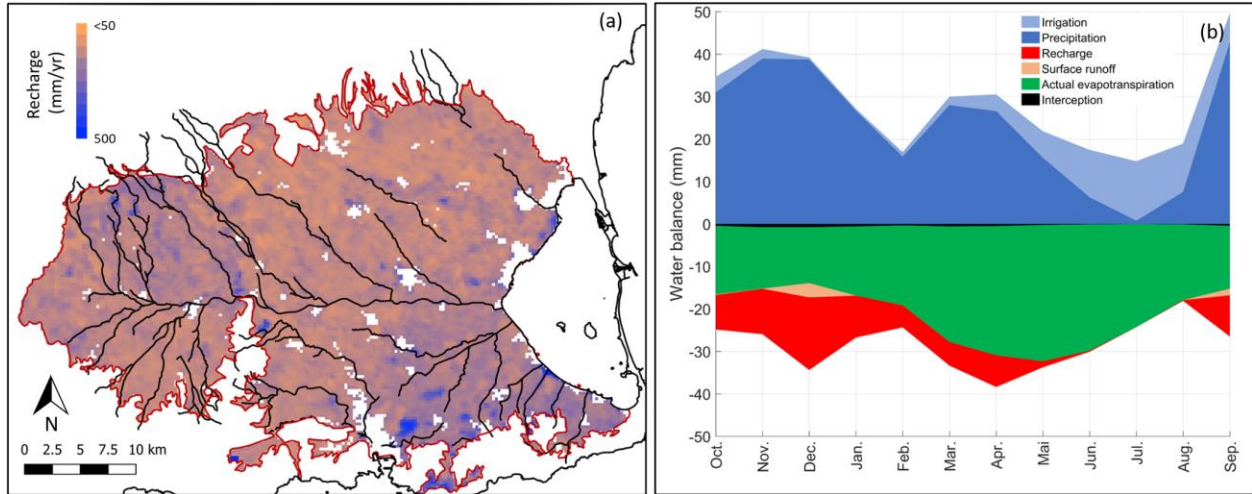
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974 **Figure 7:** (a) Spatial distribution of estimated mean annual recharge (mm/yr); (b) Monthly averaged water
 975 mass balance components for the study period (2000-2016), i.e., precipitation and irrigation as
 976 inflows, and actual evapotranspiration, surface runoff, interception and recharge as outflows.

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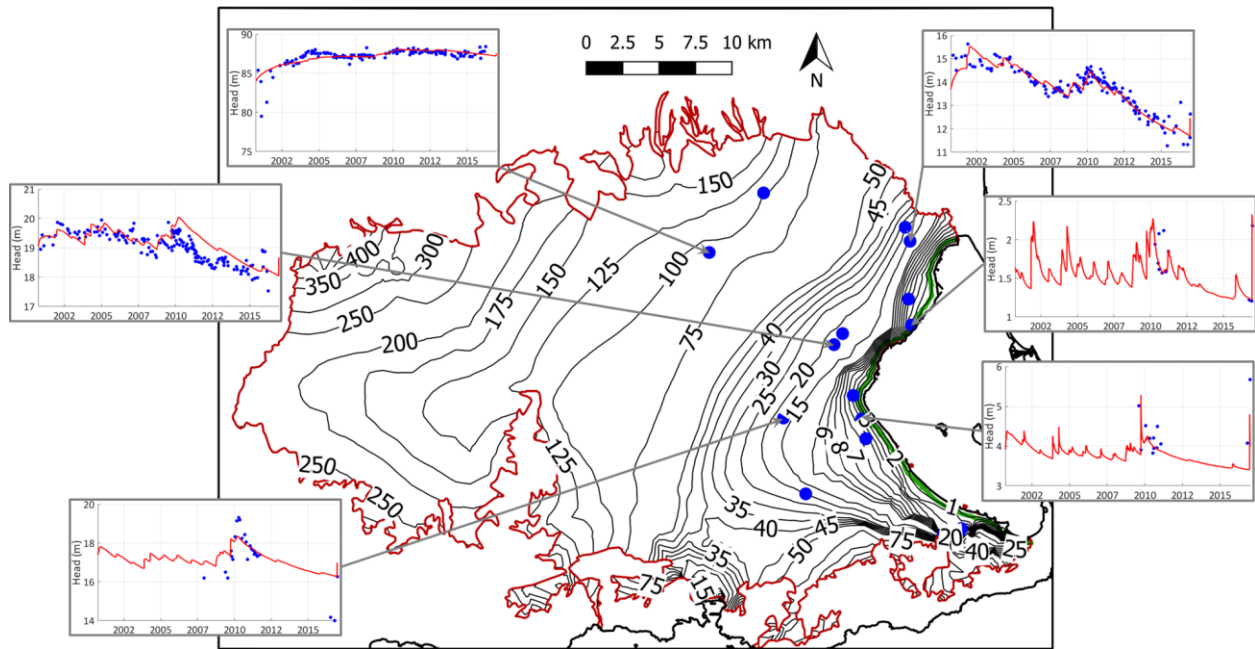
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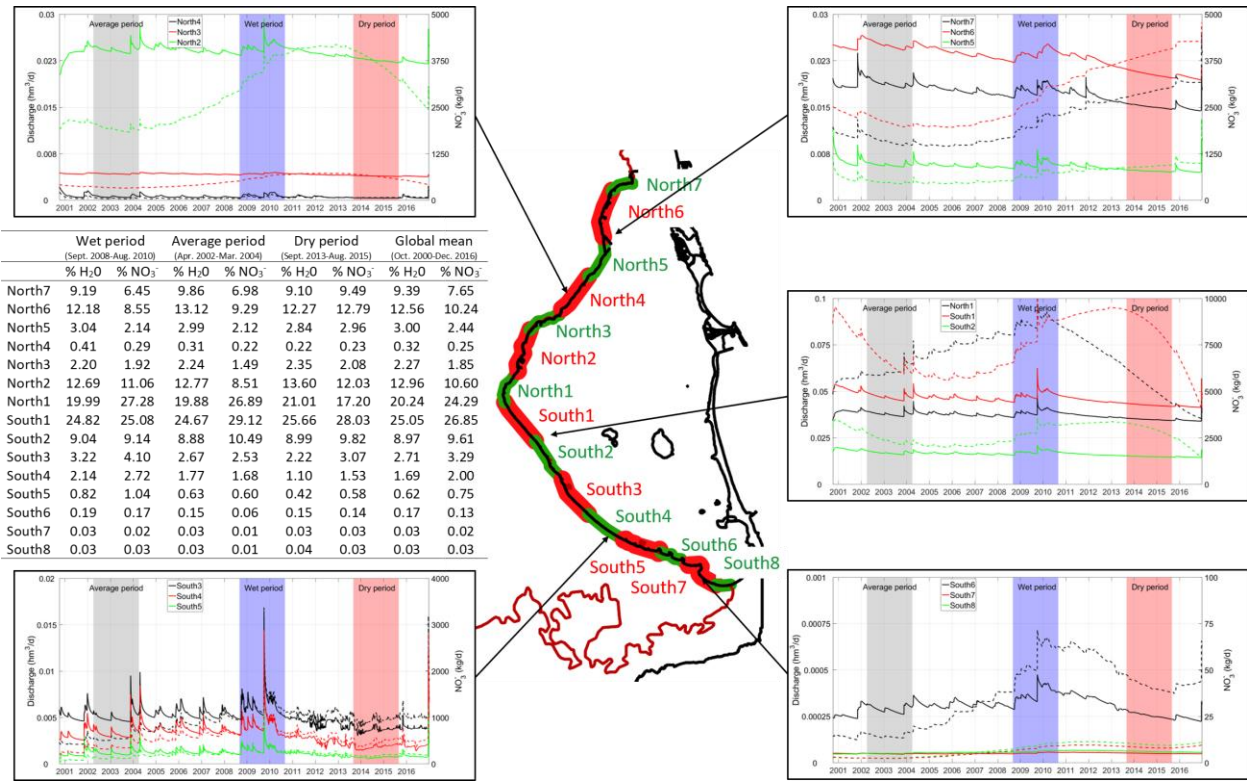
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984 **Figure 8:** Contours of the hydraulic heads from the calibrated model at date 15/03/2004, after a two-year
 985 hydrometeorological average period: (1) head isolines (black lines; note that isolines are not
 986 equidistant); (2) mean penetration of the saltwater wedge at aquifer bottom (green line). The insets
 987 depict the temporal evolution of calculated hydraulic heads (red lines) and available
 988 measurements for model calibration (blue points) at selected observation wells.

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990

991 **Figure 9:** Spatio-temporal distribution of discharge of groundwater and nitrate into the Mar Menor lagoon.

992 The perimeter of the lagoon is divided into 15 segments with length ~2 km. For each segment,

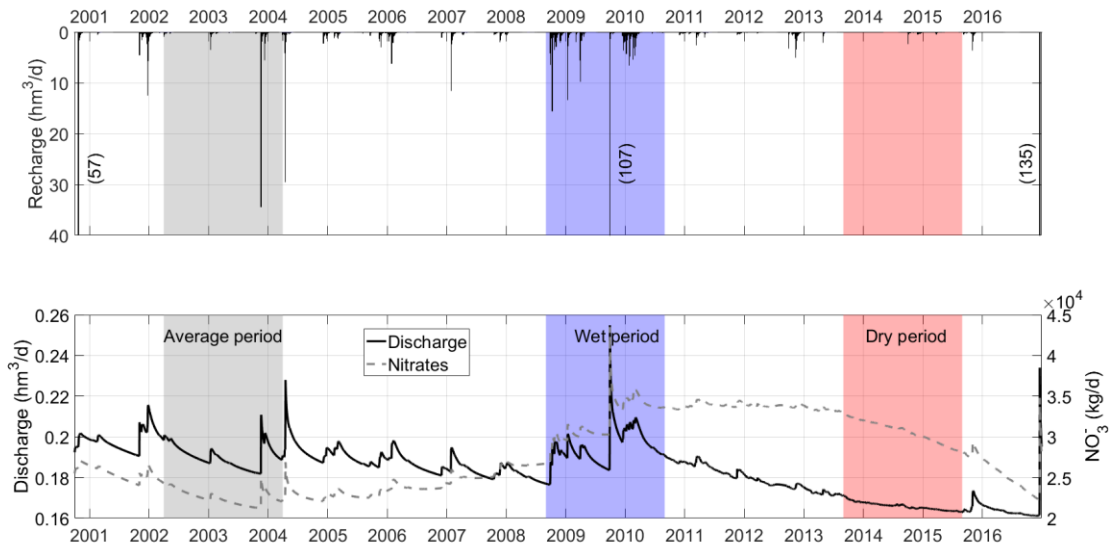
993 the discharge of groundwater (solid lines) and nitrate (dashed line with same colour) are

994 presented. Periods of average (grey), wet (blue), and dry (red) hydrometeorological conditions

995 are highlighted. The table contains, for each sector, the percentage of the mean discharge of

996 groundwater (%H₂O) and nitrates (%NO₃⁻) for selected hydrometeorological periods.

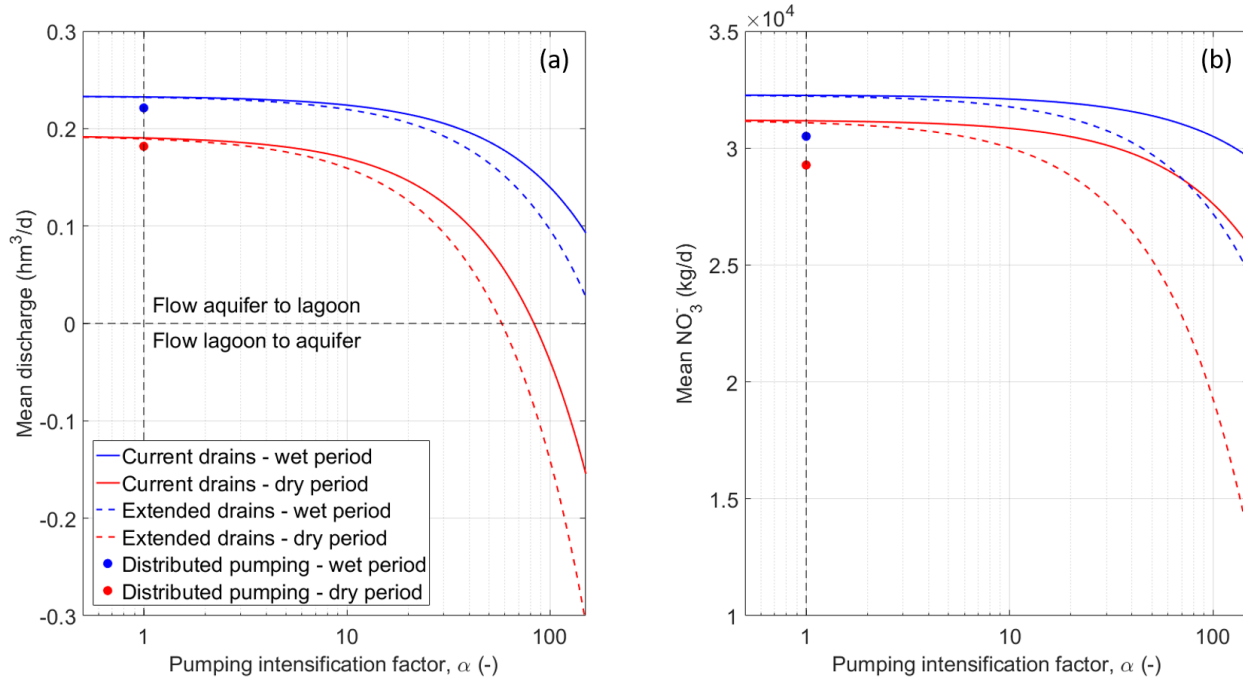
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999 **Figure 10:** (a) Daily total recharge over the entire aquifer estimated by SPHY. The vertical axis has been
 1000 trimmed to show the variation among the smaller recharge peaks. Values in parentheses
 1001 correspond to the three highest recharge values that are out of scale; (b) Daily total discharge of
 1002 groundwater (solid black line) and potential nitrate load (dashed grey line) into the lagoon.
 1003 Representative average (Apr. 2002–Mar. 2004), wet (Sept. 2008–Aug. 2010) and dry (Sept.
 1004 2013–Aug. 2015) hydrometeorological periods are shaded.

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1007 **Figure 11:** Potential discharge of groundwater (a) and nitrate (b) into the lagoon under different
 1008 management scenarios. Discharge is shown as a function of the pumping intensification factor
 1009 during wet (blue) and dry (red) hydrometeorological periods, for simulation of the localized
 1010 strategies (scenarios 1 (continuous lines) and 2 (dashed lines), involving pumping from current
 1011 and current plus extended drains, respectively) and the distributed management strategy (scenario
 1012 3).

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